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### Summary

Powers from a total of up to 120 Gunn diodes were combined at 23 GHz by combining three or five or seven 12- or 24-device Kurokawa oscillators through short-slot couplers in conjunction with high-level injection locking. Overall power combining efficiencies were 76-91 percent.

### Introduction

It has been shown possible to combine, say, up to 30-40 devices at X-band frequencies<sup>1,2</sup> by the single-cavity multiple-device techniques of Kurokawa-Magalhaes<sup>3</sup> and of Harp-Stover.<sup>4</sup> Powers from several units of these multiple-device oscillators can be combined further by appropriate methods to increase the total number of devices combined.<sup>5,6,7</sup> This paper presents results of an experiment on combining powers from up to 120 K-band Gunn diodes by combining three or five or seven 12- or 24-device Kurokawa oscillators through 3-dB short-slot couplers in conjunction with high-level injection locking.

### Principles of Operation

Fig.1 illustrates the combiner network that combines  $2N+1$  oscillators with  $N$  short-slot couplers to deliver a combined power,  $P_c$ , to a matched waveguide load at a frequency,  $f_c$ , where the couplers are indicated by the heavy lines. All the oscillators are designed and built to generate their maximum powers at  $f_c$  when operated into the matched waveguide load individually.

The combiner can be adjusted to operate at a desired frequency,  $f_c$ , as follows:

First, operate the oscillator 1 alone at  $f_1 = f_c + \Delta f_1$  with  $\Delta f_1 = +5 \sim +10$  MHz. Second, operate the oscillators 1 through 3 and tune the oscillators 2 and 3 to make the power at the output port of the combiner maximum while keeping frequency-locked conditions maintained. When the tuning is made properly as described in Ref.5, the oscillator 2(3) reflects almost all of the injected power,  $P_1/2$ , and generates its maximum power,  $P_2(P_3)$ , simultaneously. The sum of  $(P_1/2 + P_2)$  and  $(P_1/2 + P_3)$  is obtained at the output port of the first stage coupler. A small unbalanced power is injected back into the oscillator 1,

and hence,  $\Delta f_1$  is small. Subsequently, the oscillators 4 and 5 are brought into operation and are adjusted similarly, and so on. This technique has been successfully applied to multiple-device oscillators to increase the total number of devices combined.

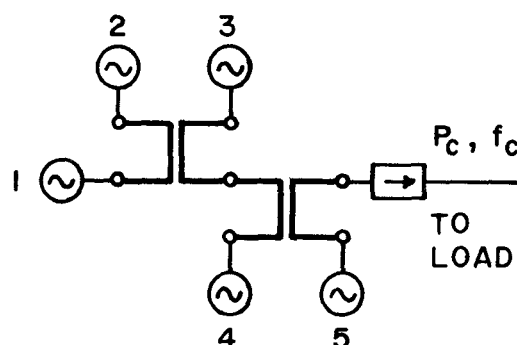


Fig.1. The  $(2N+1)$ -oscillator combining network with  $N=2$ .

### Experiments

Ten 12-device Kurokawa oscillators were built using K-band GaAs Gunn diodes (New Japan Radio Co.) and used in our experiments. The diodes were tested in a post-mount waveguide (10.7 mm x 4.3 mm) cavity and grouped into three groups according to their optimum dc-bias voltages: 4.5, 5.0, 5.5 volts. The maximum output power from a single diode was 4 to 6 mW with an average at about 5 mW. From each group, diodes were taken in dozens and mounted in Kurokawa waveguide (10.7 mm x 4.3 mm) cavity combiners. Positions of diodes and non-tapered stabilizing absorbers with respect to the waveguide cavity were adjusted and then proper output windows were selected for the maximum power, 48-72 mW, at 23.30 GHz. Power combining efficiencies at this combining stage, defined by the ratio of combined power and sum of individual diode maximum powers, were 90-93 percent. 24-device oscillators were also constructed by simply stacking pairs of the pre-adjusted 12-device oscillator modules and selecting proper output windows. The oscillation frequency was tunable over a 300-MHz range by means of a tuning screw in the waveguide cavity.

Three or five or seven  $(2N+1)$  of these multiple  $(M)$ -device oscillators were combined

through N short-slot couplers as shown in Fig.1. Results are summarized in Table 1 and in Fig.2, where  $M \times (2N+1) = 36, 60, 72, 84, 120$  diodes were combined at about 23 GHz. As described earlier,  $P_c$  approaches the sum of maximum powers from individual oscillators when tuned properly.

Table 1. Results of power combining experiments at 23 GHz using 12- and 24-Gunn-diode Kurokawa oscillators.

Exp. No.	Total No. of Diodes Combined	$M \times (2N+1)$	$f_c$ GHz	$P_c$ mW	$\eta$ %
1	36	12×3	23.46*	160	89
2	36	12×3	23.30	193	107**
3	60	12×5	23.31	242	81
4	72	24×3	23.32	323	90
5	84	12×7	23.30	382	91
6	84	12×7	23.30	362	86
7	120	24×5	23.47*	451	76
8	120	24×5	23.32	486	81

\* Oscillators were adjusted for the maximum power at 23.45 GHz.

\*\* Larger power oscillators were used.

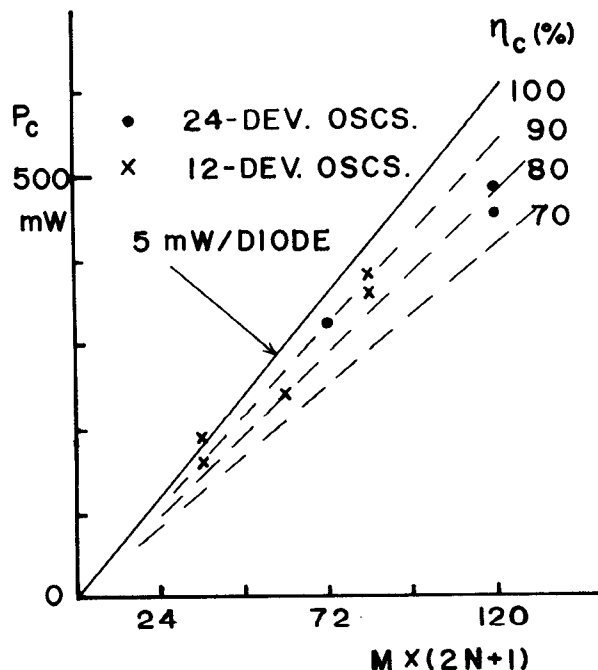


Fig.2. Combined power versus total number of diodes combined at about 23 GHz. Output power from individual diodes was about 5 mW on average.

The solid-line in Fig.2 corresponds to 5-mW per diode and can be interpreted as a

100-percent overall power combining efficiency line, roughly speaking. The 120-diode combiner, where all the diodes were biased by a common power supply, produced 486 mW at 23.32 GHz with an 81-percent overall combining efficiency. We have not tried to combine the diodes above 120 so far, but it appeared quite possible to extend the number to a 150-200 range.

Tuning characteristics of the 36-device combiner of Exp.1 in Table 1 were measured and results are presented in Fig.3. In this measurement, the combiner was first adjusted for the maximum power,  $P_{co} = 160$  mW, at  $f_{co} = 23.46$  GHz, and then the oscillator 1 alone was tuned to tune  $f_c$ . The combined power,  $P_c$ , is given as a function of the frequency difference,  $\Delta f_c = f_c - f_{co}$ , in Fig.3.

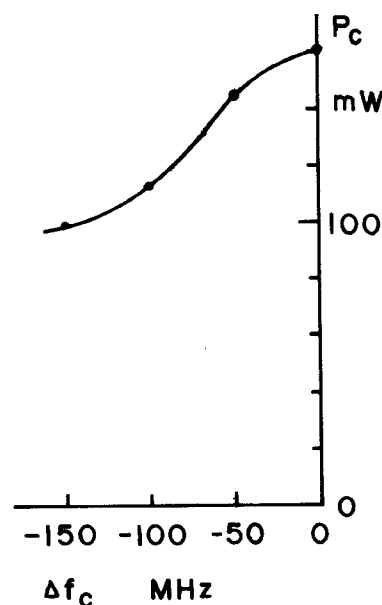


Fig.3. Tuning characteristics of the 36-device combiner of Exp.1 in Table 1.

Dependence of combiner operation on the dc-bias voltage was also measured on the same combiner. Results are represented by the  $P_c$  and  $f_c$  versus bias-voltage curves in Fig.4. Operation of all the combiners was found stable over a certain range of bias voltage when circuit adjustments were made properly.

Pulsed operation of the combiners was also found possible. An RF spectrum obtained from another  $12 \times 3 = 36$ -diode combiner operating under pulsed and primed conditions is shown in Fig.5. Conditions of the operation were: bias-voltage pulse height=6.5 volts, pulse width=2  $\mu$ s, duty ratio=10 percent, frequency=23.29 GHz, peak output power=325 mW, CW priming power=1.3 mW.

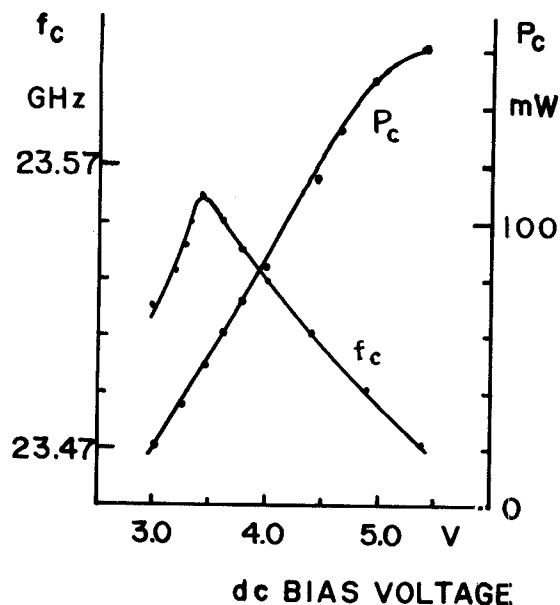


Fig.4. Combined power,  $P_c$ , and frequency,  $f_c$ , versus dc-bias voltage for the 36-device combiner of Exp.1 in Table1.

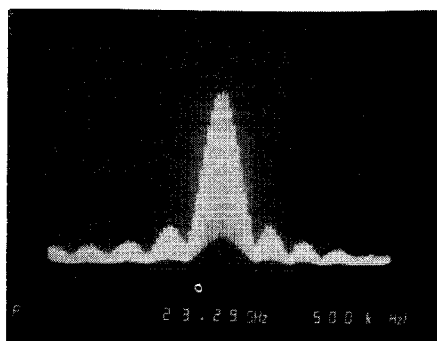


Fig.5. An RF spectrum of a  $12 \times 3 = 36$ -device combiner.  
Pulse width: 2  $\mu$ s. Duty ratio: 10 %. Peak output power: 325 mW.  
CW priming power: 1.3 mW.  
Frequency: 23.29 GHz.  
Bias voltage pulse height: 6.5 V.

### Conclusions

The  $(2N+1)$ -oscillator combining technique has been successfully applied to combine powers from several units of the single-cavity multiple-Gunn-diode oscillator of Kurokawa type to increase the total number of devices combined up to 120 at about 23 GHz. It appears quite possible to extend the number to a 150-200 range. The present technique will be readily applicable to other devices such as IMPATT as well as to other types of oscillators such as of Harp-Stover. Of particular interest for future works is application of the present method to millimeter waves.

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